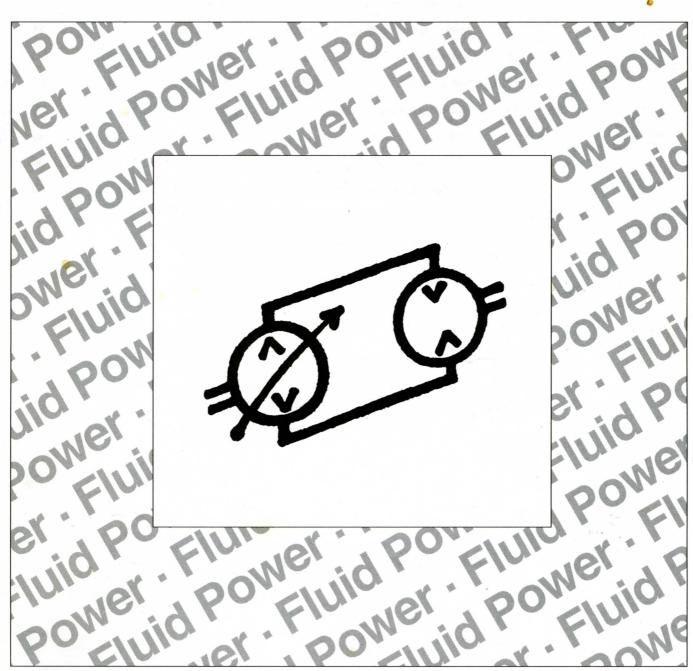


**Training material** 

# Facts worth knowing about hydraulics



DKMH.PF.000.B1.22

520L0283

Book 10 Partition 2

www.danfoss.com/fluidpower



# **Contents**

		Page
1.	Introduction	3
2.	Sizing	4
3.	Selection of components	9
4.	Selection of oil type	13
5.	Checking the oil	18
6.	Installation of system	18
7.	Starting up and running in of system	21
8.	Maintenance	. 23
9.	Fault location	24
10.	Repair and testing	. 34
11.	Symbols and tables	. 35
12.	ISO/CETOP-symbols	. 36
13.	Overview of Danfoss SERVICE SHOPS	40



#### Introduction

Like so many other technical fields, hydraulics is both old and new at the same time.

Take waterwheels for example, people have been using them since before history was recorded. On the other hand, the use of liquid under pressure to transfer force and also to control complicated movements is relatively new and has undergone its most rapid development within the last 40-50 years, not least because of the work that has been done in aeronautics.

Hydraulics and pneumatics are universal for the entire engineering industry and are amongst the three most important media for the transference and control of force. The two other media are mechanical (for example via clutch pedals and gears) and electrical (for example via a generator). "Flowing energy" is transferred and controlled through a medium under pressure - either air (pneumatic) or liquid (hydraulic).

This form of energy has many exceptional advantages and is therefore often the most suitable form of energy transference on land, sea or in the air.

A contained liquid is one of the most versatile means of controlling and transferring force. It takes the precise form of the walls that contain it and withstands its pressure. It can be divided into several streams which, depending on their size, can perform work before being allowed to merge into one stream again to perform still more work. It can be made to work fast in one part of a system and slowly in another.

No other medium combines the same degree of reliability, accuracy and flexibility while retaining the capability of transferring maximum force with minimum volume and weight. The quality control with this medium can be compared with the accuracy of an electronic micro-processor.

However, to achieve maximum utilization with highest efficiency and least possible operational stops, it is very important that a hydraulic system be designed, manufactured, started and maintained absolutely correctly. The special factors vital to the user (purchaser) must also be understood if operation in the field is not to be plagued by break downs and other disturbances.

Nearly all factory systems use "flowing energy" in production. More than half of all manufactured products are based on this form of energy, and it is therefore of interest to all manufacturers, exporters, purchasers, distributors, and repairers of production systems and machines, including agricultural machines and machine tools, the village smithy and the automobile industry, shipping and aviation.

Clearly, the knowledge and experience of many designers, producers, repairers and owners (users) is being outstripped by the dramatic development and rapid spread of hydraulics.

The purpose of this article is therefore not to try to provide patent solutions to all hydraulic problems, but to help create an understanding of why problems arise and what steps can be taken to avoid them.



Reliable sizing provides the most optimal selection of components.

It is obvious that if undersize components are used, they will not operate under overload. They will be sensitive and become a frequent source of problems and complaints. More important still, in comparison with a correctly sized component an oversize component will probably operate problem-free and "effortlessly" for a very long time, but its original price will be too high.

If not able to carry out accurate calculations to obtain optimum conditions, the guidelines below are worth following.

The first thing to establish is the max. operating pressure required for the system since this is the decisive factor in pump selection and, in turn,

important as far as the size (output) of the prime mover and the system price are concerned. The higher the operation pressure, the higher the price of many of the components.

When the economic considerations have been made, particular types and sizes of operating cylinders, motors, and steering units to be used in the system can be considered.

The pump size is found by adding the necessary amounts of oil (expressed in gallon (litres) per minute) that can be in used at the same time. Consequently, the total is the amount the pump must be able to supply at the maximum intermittent operating pressure (= pressure relief valve setting pressure).

# Size of pump

The power applied to the pump must be found as a function of the pressure in psi (bar), revolutions per minute and flow in gallon (litres) per minute, expressed in Hp. The result can be used to find the size of motor that will safely yield the necessary output. See the following example.

Hydraulic output N = pressure x flow, i.e. $N = p \times Q$ 

Example: N (HP) = 
$$\frac{p \text{ (psi)} \times Q \text{ (gpm)}}{1714}$$
 [ Hp ]

p = 2175 psi

Q = 11.9 gal/min N = 
$$\frac{2175 \times 11.9}{1714}$$
 = 15.1 Hp

When calculating the necessary pump output ( $P_{nec}$ ), account must be taken of the total pump efficiency, ( $\eta_{tot}$ ) as stated in the catalogue.

Example:

$$P_{an}(HP) = \frac{p \text{ (psi)} \times Q \text{ (gpm)}}{1714 \times \eta_{vol \text{ (eff factor)}}} = \frac{2175 \times 11.9}{1714 \times 0.9} = 16.8 \text{ Hp}$$

$$V = \frac{Q \times 1000}{n \times \eta_{vol}} \quad Q = I/min; n = min^{-1}$$

#### Sizes of pipes and hoses

The size depends on:

- max. system pressure
- max. oil flow
- length of pipe system
- environmental conditions

Pressure drop must be as small as possible. The greater the resistance in the system, the greater the operational loss. It is important to avoid those factors which cause pressure drop, for example the use of angled screwed connections. Where possible, these should be replaced by elbows. If long lengths of pipe or high flow velocity are involved, then an increase in diameter up to the next size should be considered.

Remember that the dimensions stated for the hydraulic pipes are the external diameters and wall thicknesses. The internal diameters are equal to the external diameters minus 2 x the wall thickness.

Remember that when the internal diameter is doubled, the flow area of the pipe is quadrupled. thereby reducing resistance to a quarter. Now the oil capacity supplied per minute by the pump is known, along with the amount of oil the individual components must have. The next stage is the dimensioning of pipes and hoses. This is also very important as otherwise, generated cavitation (noise), heat generation, pressure drop and, in some cases, bursting can occur.

There are many people who are frightened of this dimensioning as they associate it, incorrectly, with difficult mathematical calculations. In actual fact, if the nomogram adjacent is followed when calculating pipe dimensions, it is incredibly simple.

In order to use the nomogram, the first thing is to know the oil flow in gallons per minute. After this it has to be known whether the pipes and hoses in question are to be used as suction lines, pressure lines or return lines. This is because there are some recommended velocities of oil flow available for these categories. These values are as follows:

- Suction line 1.6 4.9 ft/sec
- Pressure line 9.8 32.8 ft/sec
- Return line 6.6 16.4 ft/sec



#### Using the nomogram

Place a ruler over the two outer columns, i.e. the known oil flow and the required speed (velocity) for the pipe type in question. Read off the nearest internal pipe diameter on the middle column. (See example page 7).

Depending on the maximun pressure, a decision can also be made as to whether to use light or heavy hydraulic pipes and hoses. Here a large price difference is involved, especially with the associated fittings. See table of pipe dimensions and max. working pressure.

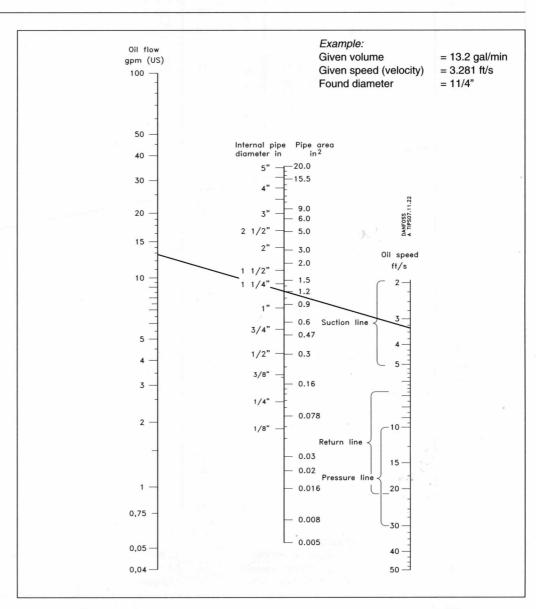
#### Valves

Valves are used in all hydraulic systems. In simple systems maybe only a pressure relief valve (safety valve) and a single directional valve are used. Other systems might be more complicated and might involve a large number and wide variety of electronically controlled proportional valves.

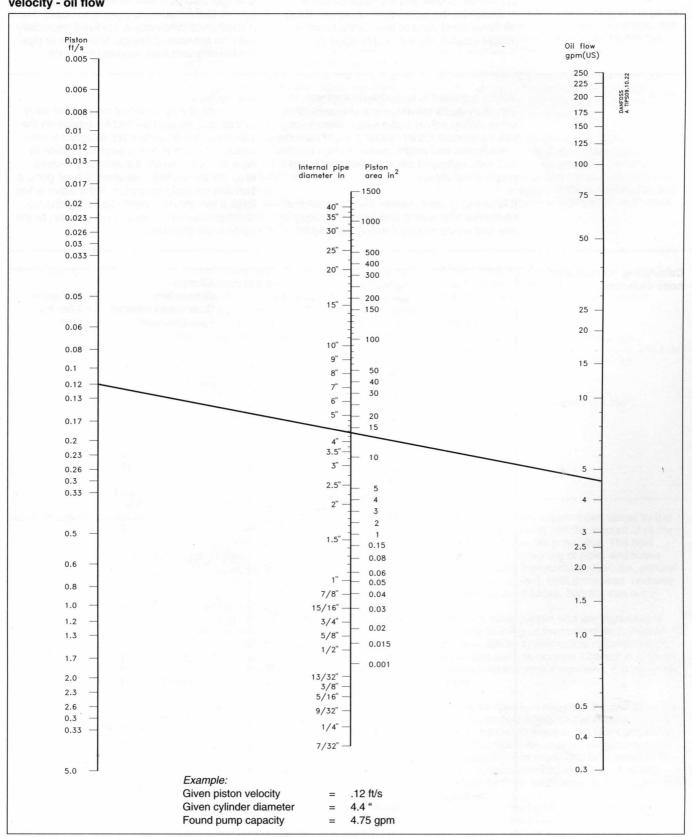
It is probably within valves that the choice of components is widest and where it is easy to use and waste money if wrong selections are made.

If in doubt, the suppliers of recognized valve brands can be approached for advice on the selection. It is important not to select a valve which is too small or too large in relation to flow. If it is too small, the relative pressure drop will be too high, resulting in heat generation and possibly cavitation. If the valve is too large it can result in poor regulating characteristics where the cylinder will pulsate, or the system will oscillate.

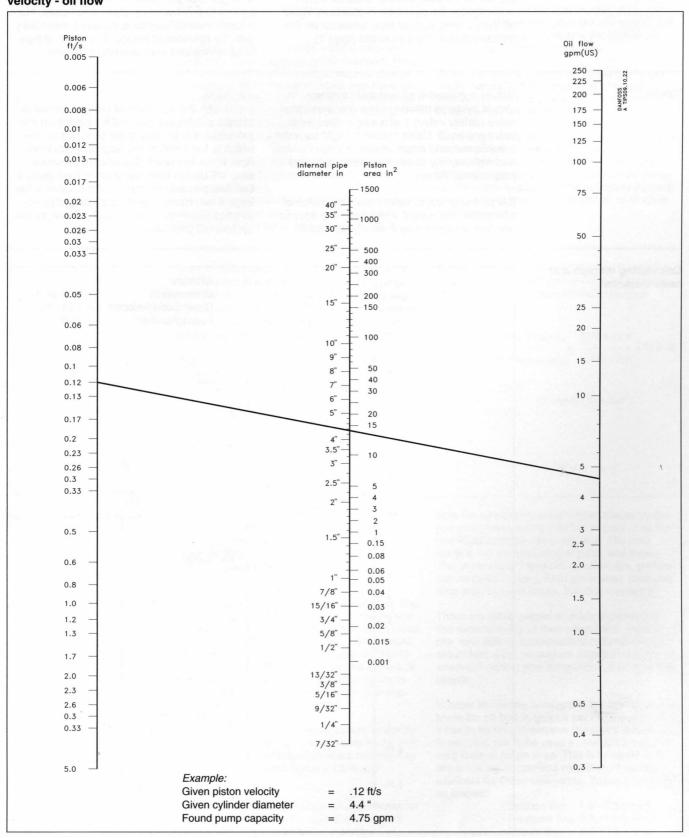
# Calculating on pipe and hose diameter



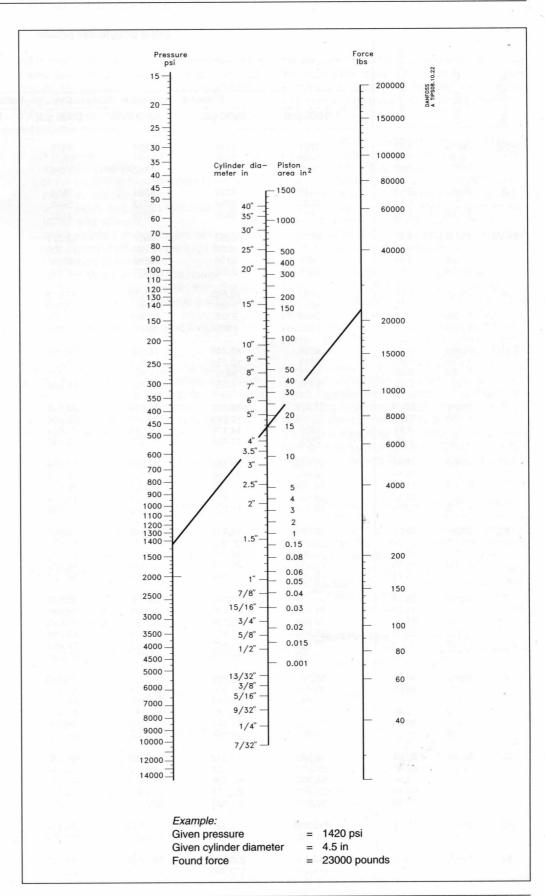
# Calculation of piston velocity - oil flow



# Calculation of piston velocity - oil flow



Calculation of cylinder force





lns.	JS.	Rod Dia., Ins. Effec. Area, Sq.Ins			Table of cyli	lider power		
Dia., I	Jia., Ir	Area		Pressure	Differential Ac	ross Cylinder F	Ports	
Bore Dia., Ins.	Rod Dia., Ins.	Effec.	1000 psi	1500 psi	2000 psi	2500 psi	3000 psi	4000 psi
I-1/2	None	1.77	1767	2651	3534	4418	5301	7068
	5/8	1.46	1460	2190	2921	3651	4381	5841
	1	.982	982	1473	1963	2454	2945	3927
2	None	3.14	3142	4712	6283	7854	9425	12,566
	1	2.36	2356	3534	4712	5890	7069	9425
	1 - 3/8	1.66	1657	2485	3313	4142	4970	6627
2 - 1/2	None	4.91	4909	7363	9817	12,271	14,726	19,635
	1	4.12	4123	6188	8247	10,308	12,370	16,439
	1 - 3/8	3.42	3424	5136	6848	8560	10,271	13,695
	1 - 3/4	2.50	2503	3755	5007	6259	7510	10,014
3	None	7.07	7069	10,603	14,137	17,672	21,206	28,274
	1	6.28	6283	9425	12,567	15,708	18,850	25,133
	1 - 3/8	5.58	5584	8376	11,167	13,959	16,751	22,335
	1 - 3/4	4.66	4663	6995	9327	11,658	13,990	18,653
3 - 1/4	None	8.30	8296	12,444	16,592	20,740	24,837	33,183
	1 - 3/8	6.81	6811	10,216	13,622	17,027	20,433	27,244
	1 - 3/4 2	5.89 5.15	5891 5154	8836 7731	11,781 10,308	14,726 12,886	17,672 15,463	23,562 20,617
	2	5.15	5154	7731		12,000	15,463	20,017
4	None	12.57	12,567	18,851	25,134	31,418	37,701	50,268
	1 - 3/4	10.16	10,162	15,243	20,323	25,404	30,485	40,647
	2	9.43	9425	14,138	18,851	23,564	28,276	37,702
	2 - 1/2	7.66	7658	11,487	15,317	19,146	22,975	38,292
5	None	19.64	19,635	29,453	39,270	49,088	58,905	78,540
	2	16.49	16,493	24,740	32,987	41,234	49,480	65,974
	2 - 1/2	14.73	14,726	22,089	29,453	36,816	44,179	58,905
	3	12.57	12,566	18,850	25,133	31,416	37,699	50,266
	3 - 1/2	10.01	10,014	15,021	20,028	25,035	30,042	40,056
6	None	28.27	28,274	42,411	56,548	70,685	84,822	113,090
	2 - 1/2	23.37	23,365	35,048	46,731	58,413	70,096	93,461
	3	21.21	21,205	31,808	42,411	53,014	63,616	84,822
	3 - 1/2	18.65	18,653	27,979	37,306	46,632	55,959	74,612
	4	15.71	15,708	23,562	31,416	39,270	47,124	62,832
7	None	38.49	38,485	57,728	76,970	96,213	115,455	153,940
	3	31.42	31,416	47,125	62,833	78,541	94,294	125,666
	3 - 1/2	28.87	28,864	43,296	57,728	72,160	86,592	115,456
	4 4 - 1/2	25.92 22.58	25,919 22,581	38,879 33,872	51,838 45,162	64,798 56,453	77,757 67,743	103,676 90,324
	5	18.85	18,850	28,275	37,700	47,125	56,550	75,400
8	None	50.27	50,265	75,398	100,530	125,663	150,795	201,060
Ü	3 - 1/2	40.64	40,644	60,966	81,288	101,610	121,932	162,576
	4	37.70	37,699	56,549	75,398	94,248	131,097	150,796
	4 - 1/2	34.36	34,361	51,542	68,722	85,903	103,083	137,444
	5	30.63	30,630	44,945	61,260	76575	91,890	125,520
	5 - 1/2	26.51	26,507	39,761	53,014	66,268	79,521	106,028
10	None	78.54	78,540	117,810	157,080	196,350	235,620	314,160
	4 - 1/2	62.64	62,636	93,954	125,272	156,590	187,908	250,544
	5	58.91	58,905	88,358	117,810	147,263	176,715	235,620
	5 - 1/2	54.78	54,782	82,173	109,564	136,955	164,346	219,128
	7 °	40.06	40,055	60,083	80,110	100,138	120,165	160,220
12	None	113.1	113,100	169,650	226,200	282,750	339,300	452,400
	5 - 1/2	89.34	89,342	134,013	178,684	223,355	268,026	357,368
14	None	153.9	153,940	230,910	307,880	384,850	461,820	615,760
	7	115.5	115,455	173,183	230,910	288,638	346,365	461,820



All hydraulic systems consist in principle of the same basic components, but just as with electronics, the combinations are infinite and the range of components immense.

Which components are the most important in a system?

- ....is it the cylinder or the motor that is going to perform the work,
- ....or the liquid (oil) that transfers force to the motor or cylinder,
- ... or the pipes and hoses that lead oil to motor and cylinder,
- ....or the valves that control the oil flow paths,
- ....or the pump that applies energy and movement to the oil,
- ....or the motor that drives the pump,
- ....or the filter that removes dirt from the oil,
- ....or the oil cooler that ensures a suitable oil temperature,
- ....or the tank that contains oil for the system..

The answer must be that specific demands are made on all these components and since none of them can be allowed to fail, they must all be equally important. Therefore extreme care must be taken in all stages of their creation, selection and application.

When a hydraulic diagram is being prepared,

the designer must have quality in mind, including the quality of the drawing itself, so that any errors in interpreting the drawing are avoided. It is a good idea always to use the correct ISO/CETOP-symbols.

When the diagram is subsequently used in preparing parts lists and accurate component specifications, sizing problems often occur. The designer is confronted with brightly coloured brochures and catalogues and, at first, all is confusion. The temptation is to revert to rule-of-thumb methods and "add a bit for safety's sake", the result being a system which is either over or under designed.

All reputable hydraulic component manufacturers give real, usable values in their catalogues, not just theoretical desired values. The technical data in Danfoss catalogs always represents average values measured from a certain number of standard components. In addition to these data, the catalogs contain a mass of useful and explanatory information on selection, installation and start up of components, together with a description of their functions. This information must, of course, be used as intended in order to avoid overload, too high a wear rate, and consequent oil overheating and to avoid an over-dimensioned system with poor regulation at too high a price.

#### The tank

Let us look a little closer at an example system, starting with:

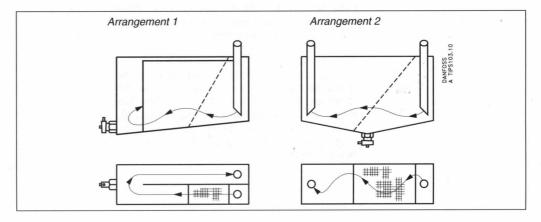
The tank, which has many functions e.g.

- as a reservoir for the system oil
- as a cooler
- as a "coarse strainer", sedimentation of impurities
- as an air and water separator
- as a foundation for pumps etc.

The dimensions of the tank and its form are important and it should therefore be designed

for its purpose, the same as all other hydraulic components. Its location must also be taken into account so that the sight glass, filters, filling cap, air filter, drain cock, etc. are easily accessible for daily inspection. If the application is mobile, if there is no cooler built into the system, and provided the tank is located where air circulation is good, the size of the tank can be fixed at approx. 3-4 times the capacity of the pump per minute.

Two arrangements are shown below. Arrangement 1 is preferred as this increases the cooling effect as much as possible.





To increase the ability of the tank to separate dirt and water, the bottom must be slightly inclined (deepest end opposite the inlet/outlet end). An ordinary cock (without handle) is fitted so that impurities can easily be drained off. Increased separation of the air that is always present in the oil can be obtained by fitting an inclined coarse metal strainer (approx. 25-50 mesh/ inch) by the return line.

Both suction and return pipes must be cut diagonally. The ends of the pipes must be located 2-4 times the pipe diameter above the bottom of the tank, partly to avoid foaming at the return line, and partly to prevent air from being drawn into the suction line, especially when the vehicle/vessel heels over to one side. With regard to the annual "spring-clean", the tank must have large removable covers, either in the sides, in the top, or in the ends, in order to give easy access for cleaning. If filters are installed, they must be located above the tank oil level and must be easy to replace without significant spillage. That is to say, it must be possible to place a drip tray under the filter inserts.

Since tanks are made of steel plate, rust is inevitable (even below the oil level, because oil contains both water and oxygen) and it is therefore advisable to surface-treat the inside. If the tank is to be painted, thorough cleaning and degreasing is necessary before primer and top coats are applied. The paint used must, of course, be resistant to hot hydraulic oil

If the cooling effect from the tank and other hydraulic components is insufficient in order to keep oil temperature down to an acceptable maximum an oil cooler must be fitted. Most suppliers prescribe 194°F (90°C) as an absolute maximum partly because of lifetime of rubber parts, partly because of alterations of tolerances and possibly bad lubrication. Today quite often electronic devices are fitted directly onto the hot hydraulic components. In consideration of the electronics, a reduction of the max. oil temperature to under 176°F (80°C) must be aimed at.

#### **Filters**

The degree of filtering and filter size are based on many different criteria that generalisation is seldom possible. The most important factors to be considered are as follows:

#### Operational environment:

How serious would the consequences be if the system failed because of dirt?

#### Oil quantity:

Would there be a few litres or several hundred litres in the system? Is it an expensive or a cheap oil?

#### Operational down time:

What would it cost per hour/day if the system shut down? How important is this factor?

#### Dirt sensitivity:

How dirt-sensitive are the components? What degree of filtering is recommended by the component manufacturers?

#### Filter types:

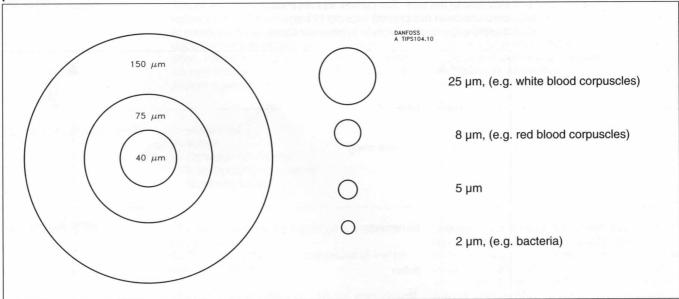
Are suction filters, pressure filters or return filters to be used, or a combination of these with or without magnets? Is exclusive full-flow filtering involved, or will there also be by-pass filtering through fine filters? Which type of dirt indicators are to be used, visual, mechanical or electrical?

#### Air filtration:

Air must be filtered to the same degree as the finest filter in the system, otherwise too much dirt can enter the tank with the air. If there is a large differential or plunger cylinders are in the system, the tank breathes in/pushes out large amounts of air, therefore the size of the air filter must be on the large side. Remember that dirt particles visible to the naked eye (larger than 40  $\mu m$ ) are as a rule, less dangerous than those that cannot be seen. It is often the hard particles of 5 - 25  $\mu m$ , corresponding to normal hydraulic component tolerances, that are the most dangerous.







The naked eye is unable to see objects smaller than 40  $\mu m$ .

For normal operation, the degree of filtration for hydraulic products can generally be divided into the categories below:

#### Motors:

25,um nominal - degree of contamination 20/16 (see ISO 4406) for return filter, or combined with a magnetic insert if a coarser filter is used, e.g. 40  $\mu$ m.

#### Steering units:

For systems having an efficient air filter and operating in clean surroundings, 25  $\mu$ m nominal is adequate. If this is not the case 10  $\mu$ m absolute - to 19/16 must be fitted. Filters can be either pressure or return filters.

# Proportional valves:

#### System filters

Where demands for safety and reliability are very high a pressure filter with bypass and indicator is recommended. Experience shows that a 10  $\mu$ m nominal filter (or finer) or a 20  $\mu$ m absolute filter (or finer) is suitable. It is our experience that a return filter is adequate in a purely mechanically operated valve system.

The fineness of a pressure filter must be selected as discribed by the filter manufacturer so that a particle level 19/16 is not exceeded.

### Radial piston pumps:

In open as well as closed systems:

#### Suction filter:

100  $\mu m$  nominal or finer, but not finer than 40  $\mu m$  nominal.

#### Return filter:

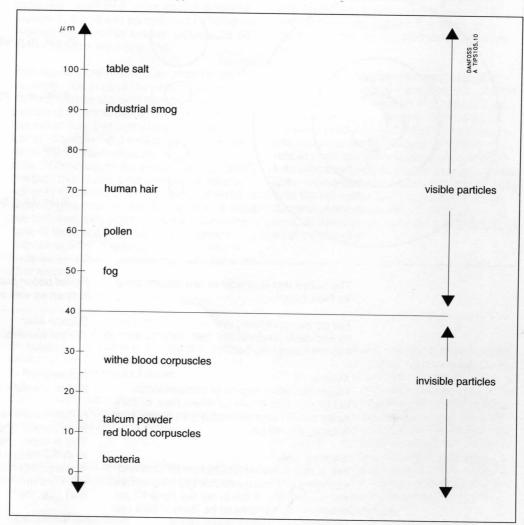
20 μm absolute or 10 μm nominal - 19/16.

Filters should be fitted with a dirt indicator so that operating conditions can be observed. This is especially important with suction filters to avoid pressure drop in the suction line and consequent cavitation. The pressure in the suction line must not be less than 11.6 psi (0.8 bar) absolute.



#### **Dimensions**

Remember that drain lines from valves, motors etc. must also be routed through the return filter to the tank. For pumps, the drain oil pressure must not exceed 14.5 psi (1 bar), therefore the drain oil should bypass the filters.





# Selection of oil type

#### Oil requirements

The oil in a hydraulic system must first and foremost transfer energy, but the moving parts in components must also be lubricated to reduce friction and consequent heat generation. Additionally, the oil must lead dirt particles and friction heat away from the system and protect against corrosion.

- good lubricating properties
- good wear properties
- suitable viscosity
- good corrosion inhibitor
- good anti-aeration properties
- reliable air separation
- good water separation

#### Types of hydraulic fluids

- Mineral oil
- Water
- Oil/water-emulsions
- Water/polyglycol mixture
- Synthetic liquids

#### Oil types

The most common hydraulic oil is a mineral based oil.

CETOP RP75H-class is comprised of the following 4 groups:

 - HH: oil without additives - HL: oil with special additives for improving fluid life-durability and protecting against corrosion - HM: "HL" + additives for improving wear-properties - HV: "HM" + additives for improving the viscosity index However, it can be an advantage to use other types of oils, especially in mobile systems such as tractors, etc. There is an advantage to be gained here from the use of the same oil for the diesel motor, the gearbox and the hydraulic system which often supply oil to both the working hydraulics and the steering. Other systems use transmission oil for the gearbox and hydraulics. In mines and off-shore installations, fire retarding liquids are used.

#### Non-inflammable fluids

Fire retarding hydraulic oils are sometimes classified as "non-inflammable hydraulic oils", but they will all burn under unfavourable conditions.

In water-based hydraulic oils it is solely the water that makes them fire retarding. When the water has evaporated, they can burn. Among synthetic fire retarding hydraulic oils, only phosphate esters are used.

It is important to select an oil type containing the correct additives, i.e. those which match the problem-free operation and long operating life for both hydraulic components and the oil itself can be ensured by following the maintenance instructions.

#### **Additives**

To improve the characteristics of a mineral oil, different kinds of additives are used. Normally the desire is to improve the following characteristics:

- Lubrication with metal/metal contact at high and low speeds.
- Viscosity change must remain small in a wide temperature and pressure range. This characteristic is called the viscosity index (VI)
- Air solubility must be low and air emission high.
- Foaming tendency must be low.
- Rust protection must be high.
- The toxicity of the oil and its' vapour must be low.

The amount and type of these additives are seldom given by suppliers, for such precise data are hardly of significance. The exception however, is antiwear additives because these are important as far as avoiding seizing and prolonging the operating life of the system. In the opinion of Danfoss, the ideal oil contains:

either: 1.0-1.4% Dialkylzincdithiophosphate (tradename Lubrizol 677A)

or : 1.0-1.6% tricresylphosphate (tradename Lindol oil)

or : 1.0-1.6% Triarylphosphate (tradename Coalite)

or : additives producing similar effects.



# Selection of oil type

Motor oil

Motor oils and most transmission oils contain self-cleaning additives. These are a disadvantage in hydraulic systems.

For example, water condensed from the oil

cannot be drained off; it forms an emulsion with the oil. This in turn leads to filters becoming clogged too quickly.

Viscosity classification system

The International Organisation for Standardisation (ISO) has developed a system viscosity classification system for industrial lubricating oil which Shell and the other large oil companies have decided to introduce (ISO 3448)

## Viscosity diagram

ISO Viscosity No.				ty limits in mm <sup>2</sup> /s (40°C)
		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Minimum	Maximum
ISO VG	2,00	2,20	1,98	2,42
ISO VG	3,00	3,20	2,88	3,52
ISO VG	5,00	4,60	4,14	5,06
ISO VG	7,00	6,80	6,12	7,48
ISO VG	10,00	10,00	9,00	11,00
ISO VG	15,00	15,00	13,50	16,50
ISO VG	22,00	22,00	19,80	24,20
ISO VG	32,00	32,00	28,80	35,20
ISO VG	46,00	46,00	41,40	50,60
ISO VG	68,00	68,00	61,20	74,80
ISO VG	100,00	100,00	90,00	110,00
ISO VG	150,00	150,00	135,00	165,00
ISO VG	220,00	220,00	198,00	242,00
ISO VG	320,00	320,00	288,00	352,00
ISO VG	460,00	460,00	414,00	506,00
ISO VG	680,00	680,00	612,00	748,00
ISO VG	1000,00	1000,00	900,00	1100,00
ISO VG	1500,00	1500,00	1350,00	1650,00



# Checking the oil

#### Water in the oil

There is evidence that more than 70% of all problems with hydraulic systems can be traced directly to the condition of the oil. If there is water in the oil, the oil must be replaced as this not only damages the ball and roller bearings but also causes corrosion of all steel surfaces. This especially applies to those surfaces touched by the oil, for in addition to

water, oxygen is present and this promotes rust. A further danger is the reduction of the operative area of filters and the consequent increase in the abrasiveness of the oil.

## Oil oxidation

Normally an oil operating temperature of 86°F-140°F (30-60°C) ought to be aimed at since the life of hydraulic oil is strongly dependent on its op-erating temperature. The rule-of-thumb is that the useful life of an oil is halved for every 46.4°F (8°C) the temperature rises above 140°F (60°C). That is to say, at 194°F (90°C) the life of the oil is only about 10% of its life at 140°F (60°C).

The reason for this is oxidation. At atmospheric pressure, all oils contain a little less than 0.1 litres of air per litre of oil. Therefore, in practice, oxygen is always present and it reacts with the hydrocarbons making up the oil. Gradually, as oxidation increases, the oil becomes darker in colour and its' viscosity rises.

Finally, the products of oxidation can no longer be dissolved in the oil, but instead settle everywhere in the system as a brown sticky layer. This will cause sticking valves and high friction in ball bearings, valve spools and pump pistons. Oxidation also produces corrosive acids.

The oxidation process begins gradually, but at a certain stage the oxidation rate suddenly rises and the viscosity rises. The resulting increase in operating temperature accelerates the oxidation process even more and soon the oil becomes quite unusable as a hydraulic oil because of deposits, high viscosity and accumulated acids. It therefore pays to take care of the oil. Even without proper laboratory equipment, many factors can be checked.

#### The presence of water

It is possible to make the following checks:

The presence of water can be detected as follows. Drain 32.8 in<sup>3</sup> or 49.2 in<sup>3</sup> (two or three cm<sup>3</sup>) of oil into a test tube and allow it to stand for a few minutes until any air bubbles have disappeared. Then heat up the oil, with a gas

lighter, for example, and at the same time listen (at the top of the test tube) for small "explosions" in the oil. This sound comes from the creation of water vapour when the small water particles in the oil are shock-boiled.

#### **Viscosity**

Viscosity can be established with sufficient accuracy using homemade equipment consisting of a small container (e.g. a can) which is able to hold 0.2 gal (¾ litre) of liquid. The bottom of the can must be pushed slightly out-wards and a burr-free hole of 0.16" - 0.2" (4 - 5 mm) drilled. Pour water which has been heated to 104 - 122°F (40 - 50°C) into the can whilst keeping a finger over the hole. Remove the finger and record in seconds how long it takes for the water to run out. Repeat the process, but this time use oil. The viscosity of the oil can be calculated in degrees Engler (E°).

Engler Viscosity =

drain time for oil
drain time for water

See conversion table page 16.



#### Checking the oil

#### The smell and appearance

The smell and appearance of an oil sample also reveals much about its condition, especially if it is compared with a sample of clean unused oil at the same temperature and in the same kind of glass container. By allowing two such samples to stand overnight, the bottom of the glass containing the used oil might reveal a deposit. If it does the oil in the system must be fine-filtered and the tank cleaned.

If these relatively crude tests indicate that the oil might be bad, small systems should scrap the oil. For larger systems an oil sample of approx. 0.132 - 0.264 gal.( $\frac{1}{2}$  - 1 liter) should be sent to a laboratory for a thorough check. Remember it is important that the bottles used for the samples are completely clean.

# Tables for converting viscosity

mm²/s	E°	R	S	mm²/s	E°	R	S
1,00	1,00	26,7	29,3	26,00	3,58	109,1	123,6
1,50	1,07	28,4	31,3	27,00	3,71	113,0	128,0
2,00	1,12	30,3	33,1	28,00	3,83	117,0	132,4
2,50	1,17	31,7	34,8	29,00	3,96	120,9	136,8
3,00	1,22	33,0	36,5	30,00	4,09	124,8	141,3
3,50	1,27	34,5	38,0	31,00	4,21	128,8	145,7
4,00	1,31	35,8	39,5	32,00	4,34	132,7	150,2
4,50	1,35	37,1	41,0	33,00	4,47	136,6	154,7
5,00	1,40	38,5	42,5	34,00	4,58	140,6	159,2
5,50	1,44	39,7	44,0	35,00	4,71	144,4	163,7
6,00	1,48	41,1	45,4	36,00	4,83	148,8	168,2
6,50	1,52	42,4	47,0	37,00	4,96	152,5	172,8
7,00	1,57	43,8	48,6	38,00	5,09	156,5	177,3
7,50	1,60	45,2	50,2	39,00	5,22	160,5	181,9
8,00	1,65	46,5	51,8	40,00	5,34	164,5	186,5
8,50	1,70	48,0	53,4	41,00	5,47	168,6	191,0
9,00	1,75	49,4	55,1	42,00	5,60	172,6	195,6
9,50	1,79	51,0	56,8	43,00	5,73	176,6	200,2
10,00	1,83	52,4	58,5	44,00	5,86	180,7	204,8
10,50	1,88	53,9	60,2	45,00	5,99	184,7	209,4
11,00	1,93	55,4	62,0	46,00	6,11	188,7	214,1
12,00	2,02	58,5	65,6	47,00	6,25	192,8	218,7
13,00	2,12	61,8	69,3	48,00	6,37	196,8	223,3
14,00	2,22	65,1	73,1	49,00	6,50	200,8	227,9
15,00	2,32	68,4	77,0	50,00	6,63	204,8	232,6
16,00	2,43	71,8	81,0	51,00	6,76	208,9	237,2
17,00	2,54	75,4	85,0	52,00	6,88	213,1	241,8
18,00	2,65	79,0	89,2	53,00	7,01	217,2	246,5
19,00	2,76	82,8	93,4	54,00	7,15	221,3	251,1
20,00	2,88	86,7	97,6	55,00	7,27	225,3	255,7
21,00	2,99	90,4	101,9	56,00	7,40	229,4	260,4
22,00	3,10	94,0	106,2	57,00	7,53	233,4	365,0
23,00	3,22	97,8	110,5	58,00	7,67	237,4	269,6
24,00	3,35	101,5	114,9	59,00	7,79	241,4	27,.2
25,00	3,46	105,2	119,2	60,00	7,92	245,5	278,0

mm<sup>2</sup>/s (cSt = Centistoke)

E° = Engler°

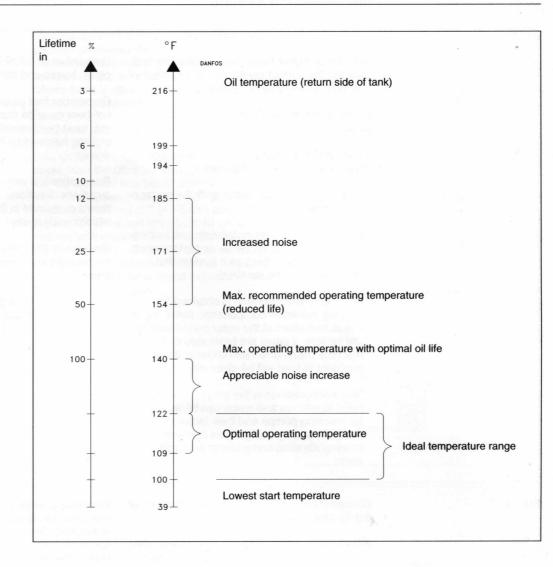
R = Redwood

S = Saybolt



# Checking the oil

Hydraulic oil life in % based on temperature conditions





# Installation of system

After the designer has made calculations and selected the correct components, a number of questions have to be considered:

Where and how are the components to be placed?

This must be in strict accordance with, amongst others, the following factors:

- Suitability in relation to the work the motor or cylinder must perform.
- Easily accessible for installation and inspection, and not least for repair or replacement.
   There is no such thing as a system that never needs to be repaired.
- Maximum heat emission is obtained by locating individual components, tanks, pipes, hoses and filters at the outer boundaries of the system. If pipes are bracketed to the machine frame or vehicle chassis, large amounts of heat will be given off.
- Noise suppression is the subject of environ ment legislation and much can be achieved by installing pumps and their motors on dampers and by using hoses between all moving/vibrating components and rigid parts.

Remember to follow catalog instructions on pipes, hoses and fittings.

Remember that pipes which are welded or hot-bent must be thoroughly cleaned. Scale etc. must be cleaned by wire brushing or by pickling followed by thorough flushing and drying.

Remember it is very advisable to read the supplier's directions and meet the requirements contained in the installation instructions which nearly always accompany components.

Remember the three most important rules to be followed when working with hydraulics are:

- 1. CLEANLINESS
- 2. CLEANLINESS
- 3. CLEANLINESS

#### Rule 1

Concerns cleanliness during the installation of the hydraulic system.

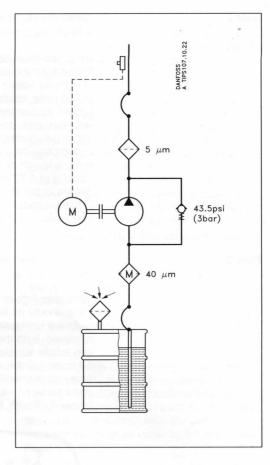
Hoses, pipes and fittings are never clean after being worked on and must therefore always be cleaned immediately prior to installation. Pipes, including pipe bends, should preferably be cleaned with a plug of crepe paper or lint-free cloth soaked in paraffin and blown through the pipe with compressed air. This process must be repeated with several plugs until a completely clean plug emerges. If pipes have been hot-bent or welded they must be cleaned by pickling in hydrochloric acid, flushed with cold and then hot water and dried. If the pipes are not to be fitted immediately, they must be lubricated with clean hydraulic oil and plugged, otherwise they will rust. The blanking plugs fitted in all pumps, motors, valves, etc. must not be removed until just before the components are installed.

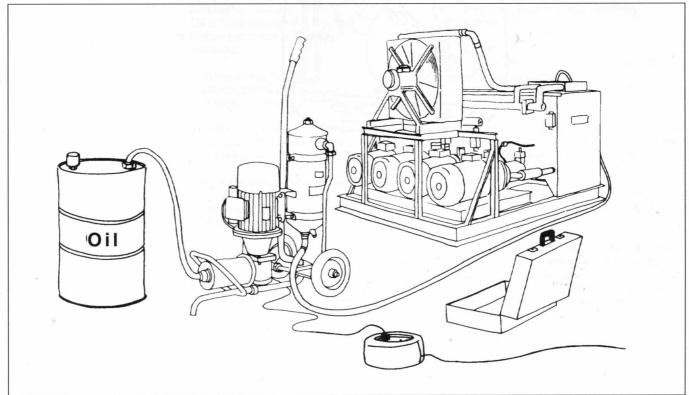
Workshops, work stations, tools and clothing must also be as clean as possible. Then there is smoking! Apart from the fire risk, tobacco ash is harmful, it acts as an abrasive. Smoking should therefore be prohibited.

#### Installation of system

Fine filtration of the oil via a filling filter unit is strongly recommended. When filling from drums there are nearly always too many par-ticles in the oil, especially in the bottom where there is often a little water too. An example of a portable filling filter unit is shown below.

It consists of a  $^34$  hp single phase electric motor driving a low pressure pump of 3.76 - 5.28 gal/min (15-20 l/min) capacity. The pump sucks from the oil drum through a pipe that can be screwed into the  $^34$  BSP drum connector. The diagonally cut end of the pipe extends to approx. 1.57" - 1.97" (4 - 5 cm) above the bottom. Oil is sucked through a 40  $\mu$ m coarse strainer with magnetic insert and then through a 5  $\mu$ m fine filter. The fine filter can be equipped with a low pressure switch that stops the pump when the filter is about to become saturated with dirt particles.







#### Installation of system

#### Rule 2

Concerns cleanliness during daily operation of a hydraulic system.

Here, the main objective is to prevent the oil from becoming dirty. That is to say, filters (including air filters) must be clean - especially piston rods, shafts and shaft seals. It has been proven that on every square centimeter of piston rod area, one dirt particle of more than  $10\mu m$  penetrates the cylinder. If we make the assumption on a piston rod of Ø 1.97 in (50 mm), a length of just 3.94 in (100 mm), and a velocity of 4.72 in/min (12 mm/min). This means about 20.000 particles larger than 10  $\mu m$  per minute! The tools used for filling must of course be

perfectly clean and the oil filled into the system must be filtered through filters of the same fineness as the finest in the system, normally 5  $\mu$ m, but in any event no coarser than 10  $\mu$ m nominal. Oil in large drums is not normally clean enough and, depending on the storage, often contains water.

Therefore drums should be laid down during storage, or better still, should stand on a slant if kept out-doors so that water cannot collect around the plugs.

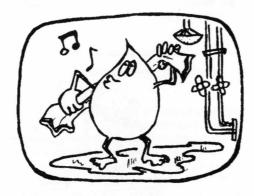
#### Rule 3

Concerns cleanliness during inspection and repair.

Here also it goes without saying that everything should be kept as clean as possible. Before a hydraulic component is removed, both the component itself and the immediate surroundings must be clean. All loose paint scale must be removed before screwed connections are dismantled and all open parts, pipes, hoses, etc. must be blanked off with, for example, plastic bags

bound on so that dirt and dust cannot enter the system when it is in standstill.

A hydraulic component must never be dismantled outdoors, but always in a closed workshop equipped with necessary facilities, special equipment and trained personnel.





# Starting up and running in of system

Correct starting up and running-in is of the utmost importance in ensuring that the system runs for a long time without problems. All to often, many systems and especially pumps "die" after only a few hours running, some after only a few minutes, because the most elementary steps have been overlooked. One example is the non-observance of the cleanliness rules before and during start-up.

But despite even the best degree of cleanliness and care during installation, the presence of dirt in a new system cannot be avoided. During running-in, wear particles will be produced from all moving parts. It is therefore important not to apply full load to the system before this dirt has been filtered out.

Let us look at our system which is fitted with a Danfoss pump type VPA and study the procedure for starting up:

- Examine the tank to make sure it is perfectly clean internally. If it is not, clean it out with a vacuum cleaner. Often during instalation, it is necessary to bore and tap a few extra holes which are not shown on the drawing.
- 2. Fill with clean oil of the correct type through a filtering unit as described on page 23. If such a unit is not available, any filling funnels, cans, hoses must be thoroughly cleaned before they are used. Oil is filled through the return filter.
- **3.** Before the pump is started, check the following:
  - a) Have all the flanges and screwed connections been tightened? (There is always one that hasn't).
  - b) Is the directional valve in its neutral position? (If it is not, the results can be catastrophic).
  - c) Is the pressure relief valve set at minimum? (The result of a leak or a malfunction is more violent at high pressure than at low pressure).
  - d) Does the pump rotate in the correct direction? (Nearly all pumps have a particular direction of rotation: clockwise or counterclockwise looking on the end of the output shaft. The direction ought to be clearly marked with an arrow. Many pumps will not withstand being rotated in the wrong direction for more than a few minutes without oil in the pump housing).

- e) Is the pump and any suction line filled with oil? (Some pumps cannot withstand being rotated for more than a few minutes
- 4. Connect a vacuum meter in the suction line, as close to the pump as possible. Connect a 3625 psi (250 bar) pressure gauge to the high pressure side of the system. Connect a 72.5 psi (5 bar) pressure gauge to the upper drain connection. Pumps with a priming pump must be fitted with a 362 psi (25 bar) pressure gauge on the priming pump take-off. If there is more than one pump on the same shaft, each pump must be fitted with these pressure gauges.
- If possible, connect the discharge side of the pump to the tank, otherwise to a 1,32 -2,64 gal (5-10 litre) container.
- Set the pump displacement to at least 40% of maximum.
- 7. Start the pump (with a combustion engine at 800-900 r/min, or with an electric motor having short-duration start/stop functions). When the pump starts to suck (oil runs into the tank or container) stop the pump and connect its pressure outlet to the high pressure side of the system.
- **8.** If the pump does not suck relatively quickly, check the following:
  - a) Is the suction line leaky?
  - b) Is there free flow in the suction line?
  - c) Does the pump rotate at all?
  - d) Is the pump set for min. 40% displacement?
- 9. Start the pump once more. Operate each directional valve for each motor or cylinder one after another, with a necessary bleeding at as low a pressure as possible. Repeat until the return oil in the tank does not foam and the motors and cylinders operate smoothly. Check the oil level frequently and refill with filtered oil.
- 10. A further frequent check: make sure that the suction pressure is at least 11.6 psi (0.8 bar) absolute, corresponding to 2.9 psi (0.2 bar) on the scale. After a short time, the drain pressure must be max. 14.5 psi (1 bar).



#### Starting up and running in of plant

- 11. Set the pump for max. displacement and the motor for max. speed (but not higher than 3150 r/min continuous) and allow the system to run unloaded for about 20 minutes, until the oil temperature has stabili zed. Reverse the direction of the motor and the travel of the cylinders frequently.
- 12. Set the individual pressure relief valves and the pump pressure control valve at the specified pressure. Any schock valves in the system must be set at approx. 435 580 psi (30-40 bar) over the constant operating pressure. Check the oil tempera ture.
- **13.** If required, the pump max. oil flow can be set using the flow limiter.
- 14. Remove the pressure gauges and vacuum meter and insert plugs in the connections. Replace filter inserts with new ones. Check the oil level.
- 15. If there is a large amount of oil (e.g. more than 26.4 gal (100 litres) in the system), an oil sample can be taken and sent to the oil supply firm for analysis.
- 16. The system can now be put to work.



N/I	nıc	ton	an	0
IVI		ten	ıaıı	CC

Nearly all hydraulic systems, stationary as well as mobile, are accompanied by operating instructions, but the issue of maintenance instructions is just as important. To be able to correctly maintain a hydraulic system, the customer (end user) must know what has to be done. The transfer of this knowledge is the responsibility of the hydraulic system manufacturer.

## Periodic inspection

The regular inspection of a hydraulic system is more economical than making repairs when a fault occurs. If a fault does occur, the whole system ought to be checked rather than just the defective component.

Regular planned preventative maintenance of the system after a certain number of operating

hours and the scheduled replacement of important seals ensures the avoidance of costly operational stops.

To avoid forgetting something, a routine following the direction of oil flow should be adopted, beginning with:

#### The tank

The oil level must be correct and the oil must be of the prescribed type and viscosity. On large systems it pays to send oil samples for analysis at regular intervals. Factors of special importance in deciding whether the oil can continue to be used are the rise in oil viscosity, the acidity number and the content of impurities. If there is no special equipment available, a lot can still be learned about the condi-

tion of the oil by looking at its color. Poor oil can be dark, it can smell rancid or burnt; or it can be yellow, unclear or milky, which indicates the presence of air or emulsified water. And of course the oil might contain free microscopic metal particles and other foreign substances.

#### The suction line

The suction line must be inspected for damage and sharp bends that reduce the bore of the pipe and create noisy cavitation. Screwed connections must be inspected for leaks and tightened if necessary.

Rubber or plastic hoses are suspect because they often become contracted by vacuum when the oil is hot. Such items should be replaced with pipes or armoured hoses.

#### The pump

The pump must be inspected for shaft seal and other leakage. If the pump is driven by V-belt, this should be examined to ensure that it is not worn and is correctly tensioned. The different circuits on the pressure side must be examined individually, following the direction of oil flow.

There must be no leaks. Look on the floor

under the vehicle for oil patches. The fingertips are good instruments for sensing faults, the ears too - by using a screwdriver or similar tool as a stethoscope, irregularities which might later cause breakdown can often be heard.

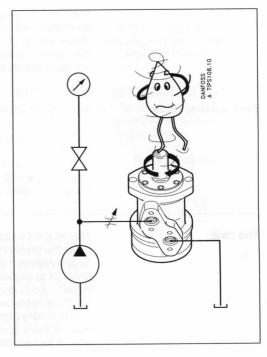
# The return line and return filter

The return line and return filter must be inspected for leaks, etc. and the filter must be checked. If the filter has a dirt indicator the condition of the filter can easily be seen. If there is no dirt indicator, the filter has to be taken out to see whether it needs cleaning or replacement.



# **Trouble shooting**

Under this heading, it is obvious that the two basic factors, pressure and flow, must be in accordance with specifications. If the opposite is true nothing will function perfectly. If the condition of the pump is suspect, the pressure line from the system must be disconnected and a pressure gauge fitted, together with a throttle valve and flow meter, as shown in the sketch below.



If no flow meter is available, a Danfoss hydraulic motor can be fitted instead. The displacement of the motor per revolution with unloaded shaft is very precise and to find flow all that is necessary is to count the number of revolutions per minute and multiply the figure by the displacement, as shown in the following examples:

Example 1: OMR 100:  
Rev./min. × disp (in<sup>3</sup>) = gpm 
$$\frac{220 \times 6.49}{231}$$
 = 5.8 gpm

Example 2: OMR 315:

$$\frac{\text{Rev./min} \times \text{disp (in}^3)}{231} = \text{gpm} \frac{116 \times 19.26}{231} = 9.64 \text{ gpm}$$

#### Pump test

Check the flow with completely open throttle valve.

Increase the throttle until it corresponds to normal operating pressure.

Again check the flow and compare it with the values given in the pump catalog.

The volumetric efficiency of the pump can be calculated thus:

$$\eta_{\text{Vol.}} = \frac{\text{flow with operating pressure}}{\text{flow with no pressure}}$$

If the capacity with operating pressure, and thereby the  $\mu$  vol. is too low, the pump has internal leakage - as a rule because of wear or seizing.

In the following, fault location is divided into three sections:

- the first section deals with hydraulic systems in general,
- the second with motors,
- and the third with systems that incorporate hydrostatic steering systems.



# Trouble shooting general

THINK before starting trouble shooting. Every fault location process should follow a logical and systematical order. Usually it is wisest to start at the beginning:

- Is the oil level correct when the pump is operating?
- Is the condition of oil and filters acceptable?
- Are pressure, flow and flow direction as specified?
- Is the oil temperature too high or too low (oil viscosity)?
- Are there any unrequired vibrations or noise (cavitation)?

If the driver of the vehicle is available ask him:

- what type of fault it is and how it affects the system,
- how long he has felt that something was wrong
- whether he has "fiddled" with the componnents
- whether he has any hydraulic and electrical diagrams available.

Diagrams are often found in the instructions included with vehicles/machines.
Unfortunately they are often so technical that they are not of much use in a fault location situation. However, the order of and the connections between the individual components are often shown.

When a defect component has, with certainty, been found both the component and its surroundings must be cleaned before removal. Loose paint must also be removed from pipes and fittings.

Holes, hoses and pipe ends must be blanked off with plugs or sealed with, for example, plasic bags after removal to avoid the entry of dirt during standstill. Never dismantle hydraulic components outside. We recommend that repairs be carried out in a workshop on a clean workbench perhaps covered with newspaper.

Make sure that a Danfoss service manual dealing with the product in question is handy. Follow the instructions word for word both when dismantling and assembling because if these instructions are not followed closely serious faults may develop.

In some cases special tools are necessary for assembling. Our service manuals give full guidance as to when this is the case.



Fault	Possible cause	Remedy
Pump noisy	No or insufficient oil supply to pump.	Clean suction filter. Check that no damage or narrowing is to be found
	2. Viscosity of oil too high.	on suction line.  2. Change the oil, adjust viscosity to working temperature.
	3. Pump takes in air:	Replace shaft seal. Tighten fittings or replace suction line. Refill with
	a) at the pump shaft b) at loose or damaged suction line c) oil level too low d) oil takes in air in the tank(return pipe discharging over oil surface)	clean oil. Extend return pipe to 54 cm under the surface and as far as possible from the suction pipe.
	<ul><li>4. Pump worn out.</li><li>5. R.p.m. too high.</li><li>6. Oil pressure too high.</li></ul>	<ol> <li>Repair or replace pump.</li> <li>Adjust the r.p.m.</li> <li>Adjust oil pressure.</li> </ol>
	and the state of t	
No pressure	Oil level too low.     Pump does not run or runs in the wrong direction.	<ol> <li>Refill with clean oil.</li> <li>Adjust direction of rotation. Check driving belt or coupling.</li> <li>Repair relief valve.</li> </ol>
	<ul><li>3. Relief valve is stuck in open pos.</li><li>4. Pump defective, broken shaft or key for rotor.</li></ul>	4. Repair pump.
No or unstable pressure	Working pressure too low.     Leaky pressure adjusting valve or pilot valve.	Check pressure adjusting valve.     Repair valve.
	3. The oil flows more or less to the tank through defective valve or cylinder.	3. Repair cylinder or valve.
		**************************************
Noise in the relief valve	1. Excessive flow.	Fit a larger valve corresponding to the actual oil volume.
	Dirt or chips between valve cone and valve seat.	2. Repair valve.
Air in the system, foam in the oil	Leaky suction line.     Excessive resistance in suction line.	Retighten or replace line.     Clean filter and suction line, or replace with pipes having larger bores. Check fittings.
	Return line discharges above the oil level - could cause foam formation.	Remove return line from suction line and extend if necessary.
	4. Incorrect oil type.	4. Change over to correct oil type.
Overheated system	No supply of cooling water.	Re-establish supply of cooling water
•	<ol> <li>Oil cooler blocked or dirty.</li> <li>Excessive oil viscosity.</li> <li>Abnormal internal leakage in one or more components.</li> <li>Altered running conditions.</li> </ol>	<ol> <li>Clean oil cooler.</li> <li>Change over to correct oil type.</li> <li>Repair or replace defective components.</li> <li>Estabiish extra cooling if necessary.</li> </ol>
	6. Pump, valves or motor overloaded.	Reduce load or replace component with a bigger one.



HYDRAULIC MOTORS	reside   Designation of the Second Se	12 (ph. 10) - 7 (ph. 10) (ph.
Fault	Possible cause	Remedy
R.p.m. of motor lower than rated value	<ol> <li>Pump worn out.</li> <li>R.p.m. of pump too low.</li> <li>Motor worn out.</li> <li>Oil temperature too high (resulting in excessive internal leakage in motor, valves etc.) Possibly too high ambient temperature.</li> <li>Insufficient diameter in pipes etc.</li> <li>Pump cavitation.</li> <li>Opening pressure of pressure relief valve too low.</li> <li>Leaky control valve.</li> <li>Overloaded motor.</li> </ol>	<ol> <li>Repair or replace pump.</li> <li>Adjust the r.p.m.</li> <li>Repair or replace motor.</li> <li>Build in oil cooler or increase existing cooler or tank capacity. If necessary change over to oil with a higher viscosity.</li> <li>Fit lines with larger diameter.</li> <li>(See under: Pump noise).</li> <li>Adjust to correct pressure.</li> <li>Repair valve.</li> <li>Eliminate the cause of the overload or change over to larger motor.</li> </ol>
Motor shaft does not rotate	Pump does not run or runs in the wrong direction.     Motor spool has seized in housing.	Start pump or reverse direction of rotation.     Replace complete shaft and housing.
	Cardan shaft or spool broken (shaft and commutator valve in two).	Replace cardan shaft or complete shaft and housing. Eliminate external forces which caused the fracture.
	<ul><li>4. Working pressure too low.</li><li>5. Sand, steel chips or similar impurities</li></ul>	4. Adjust opening pressure of relief valve to higher value, however, within permissible limits. If necessary, change over to motor with higher torque.  5. Clean the motor, and flush system
Motor shaft rotates in the wrong direction	in motor.      Oil lines are wrongly connected to motor ports.	thoroughly. Replace defective parts. Use a better filter.  1. Change the connections.
	Gear-wheel and rotary valve incorrectly fitted.	2. Adjust settings.
Leakage at motor shaft	Shaft seal worn out or cut.	Replace shaft seal.
Leak between motor spigot and housing	<ol> <li>Spigot is loose.</li> <li>O-ring defective.</li> </ol>	Tighten screws with prescribed torque.     Replace O-ring.
Leaks between housing, spacer	1. Screws loose.	Tighten screws with prescribed torque.
plate, gear wheel set and end cover, respectively	O-rings defective.     Steel washers defective	Replace O-rings.     Replace steel washers.
	5. 5.65. Macrisio dell'odivo	S. A.Spidoo diooi washioto.
	,	y - 1 A



Steering systems with OSPB-OSPC-OVP/OVR-OLS

The following quick methods of testing steering systems can be recommended:

- Start the motor (pump) and let it run for a couple of minutes.
- Drive slowly in a figure of eight. Pay special attention to any shaking or vibration in the steering wheel or steered wheels. See whether the steering wheel movements are immediately followed by a corresponding correction of the wheel movements, without any "motoring" tendencies.
- 3. Stop the vehicle and turn the steering wheel with small quick movements in both directions. Let go of the steering wheel after each movement. The steering wheel must immediately go back to the neutral position i.e. there should be no "motoring" tendencies.

4. While the vehicle is still stationary turn the steering wheel from stop to stop. Count the number of times the steering wheel turns in both directions. Note: It must be possible to turn the steering wheel with one finger.

Stop the motor (pump) and again turn the steering wheel from stop to stop. Again count the number of turns and compare with previous figures. If there is a large difference (1 turn or more) the leakage in the cylinder, gear wheel set, shock valve or suction valve is too large.

With larger vehicles where there is no emergency steering function, turn the steering wheel while the motor is idling.

5. If there is a leak, remove a hose from one of the cylinder ends and plug this and the hose. Try to turn the steering wheel again. If the wheel cannot turn the cylinder is defective. If this is not the case the steering unit or valve block is defective.



SPB - OSPC - OVP/OVR - OLS		8.10 - Authories - 3430 - 693
Fault	Possible cause	Remedy
Steering wheel is heavy to turn	1) No or insufficient oil pressure a) Pump does not run b) Pump defective c) Pump runs in the wrong direction d) Pump is worn out e) Pump is under dimensioned  2) Pressure relief valve is stuck in open	a. Start up pump (loose V-belt) b. Repair or replace pump c. Correct direction of rotation of pump or replace pump d. Replace pump e. Install a larger pump (examine pressure need and flow) 2) Repair or clean pressure relief valve.
	position or setting pressure is too low.  3) Priority valve is stuck in open posi-	Adjust the valve to the correct pressure.  3) Repair or clean the priority valve.
gresser to no nincialis allogitimo no con messo i	tion. 4) Too much friction in the mechanical pans of the vehicle.	Lubricate bearings and joints of steering gear or repair if necessary Check steering column installation.
	<ol> <li>Emergency steering balls missing.</li> <li>Combination: Downstream system + steering unit with suction valve and differential cylinder are inexpedient.</li> </ol>	<ul><li>5) Install new balls.</li><li>6) Change cylinder type (throughgoing piston rod). If necessary use two differerential cylinders.</li></ul>
Regular adjustments of the steering wheel are necessary ("Snake-like	Leaf spring without spring force or broken.	Replace leaf springs.
driving")	<ol> <li>Spring in double shock valve broken.</li> <li>Gear wheel set worn.</li> <li>Cylinder seized or piston seals worn.</li> </ol>	<ol> <li>Replace shock valve.</li> <li>Replace gear wheel set.</li> <li>Replace defective parts.</li> </ol>
Neutral position of steering wheel can- not be obtained, i.e. there is a tenden- by towards "motoring"	Steering column and steering unit out of line.     Too little or no play between stee ring column and steering unit input	Align the steering column with steerir unit.     Adjust the play and, if necessary, shorten the splines journal.
	shaft.  3. Pinching between inner and outer spools.	3. Contact the nearest service shop.
Motoring" effect. The steering wheel can turn on its own.	<ol> <li>Leaf springs are stuck or broken and have therefore reduced spring force.</li> <li>Inner and outer spools pinch, possibly due to dirt.</li> <li>Return pressure in connection with. the reaction between dfflerential</li> </ol>	Replace leaf springs.     Clean steering unit or contact the nearest service shop.     Reduce return pressure, change cylinder type or use a non-reaction control unit.
Backlash	cylinder and steering unit too high.  1) Cardan shaft fork worn or broken.	Replace cardan shaft.     Replace leaf springs.
	Leaf springs without spring force or broken.     Worn splines on the steering	Replace steering column.
, o at 2, 6, 6 <sub>0</sub> 1, 2	column.	
		****



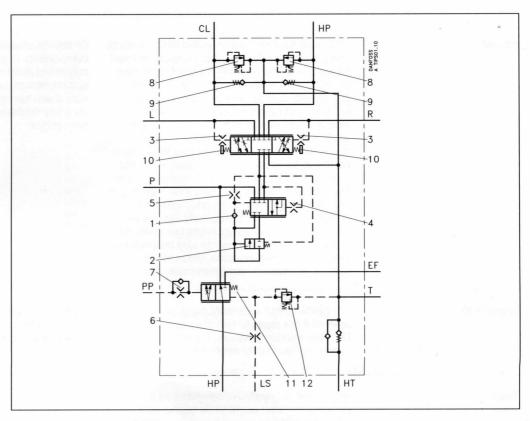
Fault	Possible cause	Remedy
Shimmy"-effect. The steered wheels ribrate. (Rough tread on tires gives vi-	1 ) Air in the steering cylinder.	Bleed cylinder. Find and remove the reason for air collection.
orations)	Mechanical connections or wheel bearings worn.	2) Replace worn parts.
Steering wheel can be turned conti- nously without the steered wheels	1) Oil is needed in the tank.	Fill with clean oil and bleed the system.
moving.	<ol> <li>Steering cylinder worn.</li> <li>Gear wheel set worn.</li> <li>Spacer across cardan shaft forgot ten.</li> </ol>	<ul><li>2) Replace or repair cylinder.</li><li>3) Replace gear wheel set.</li><li>4) Install spacer.</li></ul>
Steering wheel can be turned slowly in one or both directions without the steered wheels turning.	One or both anti-cavitation valves are leaky or are missing in OSPC or OVP/OVR.	Clean or replace defect or missing valves.
steered wheels turning.	One or both shock valves are leaky or are missing in OSPC or OVP/OVR	<ol><li>Clean or replace defective or missing valves.</li></ol>
Steering is too slow and heavy when trying to turn quickly	Insufficient oil supply to steering unit, pump defective or number of revolu tions too low.	Replace pump or increase number of revolutions.
	2) Relief valve setting too low. 3) Relief valve sticking owing to dirt. 4) Spool in priority valve sticking owing to dirt.	<ol> <li>Adjust valve to correct setting.</li> <li>Clean the valve.</li> <li>Clean the valve, check that spool moves easily without spring.</li> </ol>
	5) Too weak spring in priority valve.	5) Replace spring by a stronger There are 3 sizes: 68.2 and 145 psi (4, 7 and 10 bar).
"Kick-back" in steering wheel from system. Kicks from wheels.	1) Fault in the system.	Contact vehicle supplier or Danfoss.
Heavy kick-back in steering wheel in both directions.	Wrong setting of cardan shaft and gear wheel set.	Correct setting as shown in Service Manual.
Turning the steering wheel activates the steered wheels opposite.	Hydraulic hoses for the steering cylinders have been switched aro und.	1) Reverse the hoses.
Hard point when starting to turn the steering wheel.	Spring force in priority valve too weak.	1) Replace spring by a stronger 68.2 and 145 psi (4, 7 and 10 bar).
	<ul><li>2) Air in LS and /or PP pipes.</li><li>3) Clogged orifies in LS or PP side priority valve.</li></ul>	<ul><li>2) Bleed LS and PP pipes.</li><li>3) Clean orifices in spool and in connecting plugs for LS and PP.</li></ul>
	4) Oil is too thick (cold).	4) Let motor run until oil is warm.
Too little steering force (possibly to one side only).	Pump pressure too low.     Too little steering cylinder.     Piston rod area of the differential cylinder too large compared with piston diameter.	Correct pump pressure.     Fit a larger cylinder.     Fit cylinder with thinner piston rod or 2 differential cylinders.
	7	

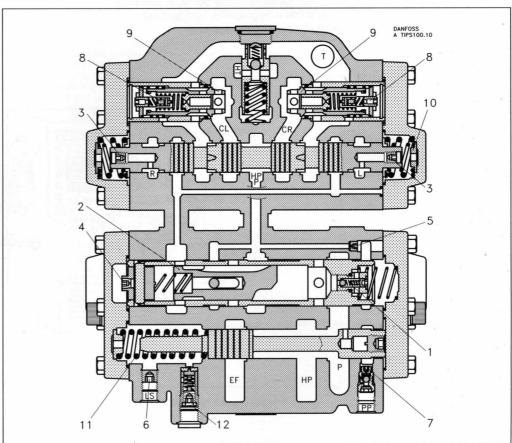


Fault	Possible cause	Remedy		
Fault eakage at either input shaft, end	Possible cause  1) Shaft defective	Remedy  1) Replace shaft seal, see Service		
over, gear-wheel set, housing or top art.	2) Screws loose.	Manual 2) Tighten screws Torque 26.4 - 31.2 lbf-in (3-3.5 daNm		
	3) Washers or O-rings defective.	OR steering unit 22.1 - 26.4 lbf-in (2,5-3 daNm).		
	of Washing of Strings acrossive.	3) Replace washers and O-rings.		
	The Thomas vices of the con-			
	control and depends on the second	a consequence of the factor and another consequence		
	er fact it fann adt all (a) do let	1 1.18.21 are to suggest which		
	polante in the golden-year. In (a) seem winty			
	Commence of the second			
		and the state of t		
	Topinistic it was			
	recent fire allocates and			
	properties to be self-refused to the			
		A.,		
	1972			
* · · · · · · · · · · · · · · · · · · ·		#		
	*			



Fault	Possible cause	Remedy		
Amplification too large	1) Dirty, leaky or missing check vave(1).	1) Clean or replace check valve.		
	2) Piston (2) sticks in the open position.	Clean and check that the piston moves easily.		
Amplification too small	1) Piston (2) sticks in the closed position. 2) Piston (2) incorrectly installed (only OSQA/B-5).	<ol> <li>Clean and check that the piston moves easily.</li> <li>Rotate the piston 180° on its axis.</li> </ol>		
Heavy turning of steering wheel and slow increase of amplification	1) Dirty orifices (3) in directional valve. 2) Dirty orifice (4) in the combi-valve spool. 3) Dirty orifice (5) in housing. 4) Dirty orifice (6) in LS-port.  (7)	<ol> <li>Clean or replace orifice.</li> <li>Clean or replace orifice.</li> <li>Clean or replace orifice.</li> <li>Clean or replace orifice.</li> <li>Clean or replace throttle/check valve.</li> </ol>		
No end stop in one or both directions	<ol> <li>5) Dirty orifice in throttle/check valve (7) in PP-port.</li> <li>1) One or both shock valves (8) set too low.</li> <li>2) One or both anti-cavitation valves (9) leaky, or sticking.</li> <li>3) Missing end-stop plate (s) (pos. 10)</li> </ol>	1) Setting takes a long time without special equipment. Contact the nearest serviceshop. 2) Clean or replace completely shock/anti-cavitation valve (s). 3) Fit end-stop plates .		
"Hard" point when starting to turn the steering wheel.	for directional valve.  1) Air in LS and/or PP pipes. 2) Spring force in the built in priority valve too weak (11).  3) Orifices in respectively LS-(6) or PP-(7) ports blocked.	1) Bleed pipes. 2) Replace spring by one which is more powerful. (There are three sizes: 68.2 - 145 psi (4, 7 and 10 bar) 3) Take out and clean orifices.		
No pressure build-up	<ol> <li>LS-pressure limitation valve (12) adjusted too low.</li> <li>Spool and sleeve in OSPBX steering unit put together incorrectly.</li> <li>Emergency control ball in steering unit missing.</li> <li>Pump does not run or is defective.</li> </ol>	<ol> <li>Remove plug and set to specified pressure.</li> <li>Take out spool set and turn the inner spool 180° in the outer sleeve. (See Service Manual).</li> <li>Install new ball.</li> <li>Repair or replace pump.</li> </ol>		
	i, i dilip dece nerran e a a a a a a a a			
Acr Pro-	Note! Fault location point denoted by number in paranthesis- see page 33.			





# Repair and testing

#### Repair

After fault location has revealed which system component is defective, that component must be removed and possibly replaced as a new or repaired one. Before removal, both the component and its surroundings must be cleaned and hoses or pipe ends blanked off with plugs or sealed with plastic bags, etc. to avoid the entry of dirt during standstill. The decision now to be made is whether the component is to be repaired domestically or by the producer. If the concerned component is from Danfoss, we recommend that it be repaired in one of our many service workshops (see list on back page). This particularly applies to more complicated components like steering units, flow amplifiers, pumps and proportional valves. For safety reasons, these all need testing with special equipment after repair.

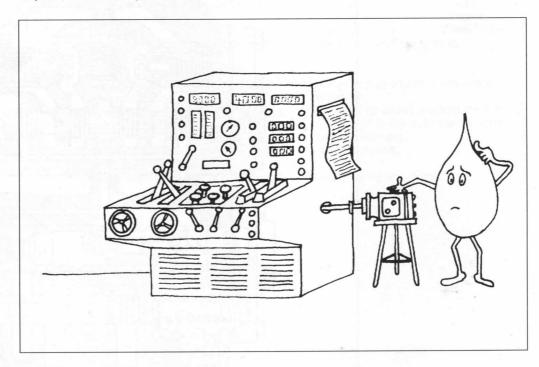
Of course situations can occur where components require immediate repair. We recommend most strongly that in such circumstances repairs be carried out only in very clean surroundings, in suitable premises on a tidy workbench perhaps covered with newspaper.

#### Important!

Dismantling and assembly must only be performed if the repairer has the associated Danfoss service manuals. If these are not followed, serious faults might develop; faults that could give rise to accidents. This is more than likely with steering components and proportional valves.

#### **Testing**

In general, all hydraulic components that have been dismantled ought to be tested on a suitable test panel to reveal possible assembly errors. If this is impossible, testing must be performed on the system.





# Symbols and Tables (SAE)

q	= Displacement	: cu in
n	= Revolutions	: rpm
p	= Pressure	: psi
Δр	= Pressure drop	: psi
Q	= Oil capacity	: gpm
V	= Speed	: ft/s
L	= Length	: ft
D	= Piston diameter	: in
d	<ul> <li>Piston rod diameter</li> </ul>	: in
D,	= Bore of pipe	: in
$D^i_h$	<ul> <li>Hydraulic diameter</li> </ul>	: in
Α	= Area	: in²
a	= Ring area	: in²
t	= Time	: sec
m	= Volume	: US gal
F	= Force	: lbf
M	= Torque	: lbf in
Р	= Power	: hp
$A_s$	= Break load	: lbf
1	= Free column length	: in
S	= Safety factor	
υ	<ul> <li>Kinematic viscosity</li> </ul>	: cSt

 Volumetric efficiency Mechanical efficiency = Total efficiency

= Resistance figure = Accumulator size

Required oil capacity available in accumulator
 Lowest oil pressure

ηt λ V<sub>ac</sub> V<sub>x</sub> P<sub>1</sub> P<sub>2</sub> P<sub>0</sub> = Highest oil pressure = Pre-charge

Ratio factors:		
Power	1 kw	= 1,36 hp
	1hp	= 75 kpm/s
		= 0,736  kw
Torque	1 kpm	= 9,81 Nm
		= 7,233 lbf ft
	1 Nm	= 0,102  kpm
Pressure	1 kp/cm <sup>2</sup>	= 98.000 Pa
	a sa	= 0.981  bar
		= 9,81 N/cm <sup>2</sup>
		= 14,22 psi
	1 psi	= 0.06895 bar
		= 0,0703 kp/cm <sup>2</sup>
	1 bar	= 1,0194 kp/cm <sup>2</sup>
Volume	1 US, gallon	= 3,785 liter
	1 Eng. gallon	= 4,546 liter
	1 in <sup>3</sup>	$= 16,38 \text{ cm}^3$
	1 liter	= 1,0 dm3
Area	1 in²	$= 645,2 \text{ mm}^2$
	1 foot <sup>2</sup>	= 92900 mm <sup>2</sup>
Speed	1 km/h	= 0,2778  m/s
×.	1 foot/s	= 0,3048  m/s
	1 mile/h	= 0,447  m/s
Acceleration	1 foot/s <sup>2</sup>	$= 0,3048 \text{ m/s}^2$
Length	1 in	= 25,4  mm
	1 foot	= 0,3048  m

Power consumption 
$$N_{an} = \frac{Q \times p}{1714 \times nt}$$
 [hp]

Supplied oil capacity Q = 
$$\frac{q \times n \times \eta v}{231}$$
 [gpm]

Input torque 
$$\qquad \qquad M \qquad = \quad \frac{q \times p}{6.28 \times \eta m} \quad [lb(f)\text{-in}]$$

#### Motor:

Oil consumption	0 -	q×n	[anm]
Oil consumption	Q =	231 × ην	[gpm]

Output torque 
$$M = \frac{q \times \Delta p \times \eta m}{6.28}$$
 [lbf-in]

Output power 
$$N = \frac{Q \times \Delta p \times \eta t}{1714}$$
 [hp]

Speed 
$$n = \frac{Q \times \eta v \times 1000}{q}$$
 [rpm]

#### Cylinder:

$$\label{eq:compressive force} \mbox{Compressive force} \quad \mbox{F} \quad = \quad \mbox{p} \times \mbox{A} \times \mbox{\eta} \mbox{m} \qquad \mbox{[lbf]}$$

Tensile force 
$$F = p \times a \times \eta m$$
 [lbf]

Speed out 
$$v = \frac{Q \times \eta v}{6 \times A}$$
 [ft/s]

Speed in 
$$v = \frac{231 \times Q \times \eta v}{720 \times a}$$
 [ft/s]

Oil consumption out 
$$Q = A \times v \times 22.71$$
 [gpm]

Oil consumption in Q = 
$$a \times v \times 22.71$$
 [gpm]

$$\begin{array}{lll} \text{Compressive force} & & & \\ \text{with differential} & & F & = & P \times (\text{A- a}) \times \eta m & [\text{lbf}] \\ \text{cut-in} & & & \end{array}$$

#### Tube:

Flow speed v = 
$$\frac{3.113 \times Q \times 100}{D^2}$$
 [ft/s]

Pressure loads in straight pipe leads 
$$\Delta p = \frac{\lambda \times L \times 0.89 \times v^2 \times 2.119}{D_i}$$
 [psi]

Resistance number: 
$$\lambda = \frac{64}{R_e} \lambda \text{ turb.} = \frac{0,316}{4\sqrt{R_e}}$$

Reynolds number 
$$R_e = \frac{v \times D_h \times 83.332}{v}$$

#### Accumulator size:

With slow charging and slow discharging 
$$V_{ac} = \frac{V_x \times \frac{P_1}{P_0}}{1 - \frac{P_1}{P_2}}$$

With quick charging and quick discharging 
$$V_{ac} = \frac{V_x \times \frac{P_1}{P_0}}{1.5}$$

With slow charging and quick discharging 
$$V_{ac} = \frac{V_x \times \frac{P_2}{P_0}}{\frac{P_2}{P_1} \frac{1}{1.5}}$$

= 0,9144 m



# **Symbols and Tables (Metric)**

q :	= Displacement		: cm³	Motor:			
	= Revolutions		: min <sup>-1</sup>			$q \times n$	
p :	= Pressure		: bar	Oil consumption	Q =		[l/min]
	= Pressure drop		: bar	The second second		$1000 \times \eta v$	
	= Oil capacity		: I/min = dm³/min				
	= Speed		: m/s	Output torque	M =	$\mathbf{q} \times \Delta \mathbf{p} \times \eta \mathbf{m}$	[Nm]
	= Length		: m	Output torque	101 —	62,8	[run]
	= Piston diameter		: mm	0.11	NI.	$\mathbf{Q} \times \Delta \mathbf{p} \times \eta \mathbf{t}$	DAM
	<ul> <li>Piston rod diame</li> </ul>	eter	: mm	Output power	N =	600	[kW]
	<ul> <li>Bore of pipe</li> </ul>		: mm			000	
	<ul> <li>Hydraulic diame</li> </ul>	ter	: mm			$Q \times \eta v \times 1000$	athensis his the
Α :	= Area		: cm <sup>2</sup>	Speed	n =		[min <sup>-1</sup> ]
a :	<ul><li>Ring area</li></ul>		: cm²			Ч	
t :	= Time		: S.	Cylinder:			
m	= Volume		: I make the second				
F	= Force		: daN	Compressive force	F =	$p \times A \times \eta m$	[daN]
	= Torque		: Nm	•			
	= Power		: kW	Tensile force	F =	$p \times a \times \eta m$	[daN]
	= Break load		: daN	Toriono Toroc		p	[aan 1]
	= Free column len	ath	: m				
		gui	. 111	Speed out	v =	$Q \times \eta V$	[m/s]
	= Safety factor	- 14	2/-	Speed out	v =	6 × A	[111/5]
	<ul> <li>Kinematic viscos</li> </ul>		: mm²/s				
	<ul> <li>Volumetric effici</li> </ul>						
	<ul> <li>Mechanical efficiency</li> </ul>	eiency				$Q \times \eta V$	1
ηt	<ul> <li>Total efficiency</li> </ul>			Speed in	v =	6×a	[m/s]
λ =	<ul> <li>Resistance figure</li> </ul>	9				6 × a	
Vac	<ul> <li>Accumulator siz</li> </ul>	e					
	<ul> <li>Required oil cap</li> </ul>	acity available in accu	ımulator	Oil consumption out	Q =	$A \times v \times 6$	[l/min]
	<ul> <li>Lowest oil press</li> </ul>			A CONTRACTOR OF THE PERSON			
	<ul> <li>Highest oil press</li> </ul>			Oil consumption in	Q =	$a \times v \times 6$	[l/min]
	= Pre-charge	54.5		C 551.1521.1.p.1.511.1.1.	_		[
0	- Tre-charge			Compressive force			
				with differential	F =	$P \times (A-a) \times \eta m$	[daN]
				cut-in	-	$1 \wedge (A^{-}a) \wedge 1/111$	[dai4]
D-41-	f			Cut-III			
	factors:	A law	1 00 h-	Tube			
Powe	r	1 kw	= 1,36 hp	Tube:			
		1hp	= 75 kpm/s			Q × 100	SHOUTHING OF
			= 0,736  kw	Flow speed v =		$6 \times D^2 \times 0.785$	[m/s]
Torqu	ie	1 kpm	= 9,81 Nm			0 × D= × 0,703	
			= 7,233 lbf ft				
		1 Nm	= 0,102  kpm	Pressure loads in		$\lambda \times L \times 0.89 \times v^2 \times$	5
Press	sure	1 kp/cm <sup>2</sup>	= 98.000 Pa	straight pipe leads	$\Delta p =$		[bar]
			= 0,981 bar	ImmenG:		D <sub>i</sub>	
			= 9,81 N/cm <sup>2</sup>				
			= 14,22 psi			64	0.316
		1 psi	= 0.06895  bar	Resistance number:	λ	$=\frac{64}{}\lambda \text{ tur}$	$rb. = \frac{0,316}{4\sqrt{Re}}$
		i poi	$= 0.0703 \text{ kp/cm}^2$	colotarioo riarribor.	,,	Re	4√ Re
		1 bar	$= 0.0703 \text{ kp/cm}^2$ = 1.0194 kp/cm <sup>2</sup>				
Malina	"11 "						
Volun	ne	1 US, gallon	= 3,785 liter	Daymalda ayaabaa	ъ	$= \frac{v \times D_h}{v}$	× 1000
		1 Eng. gallon	= 4,546 liter	Reynolds number	Re	=	
		1 in <sup>3</sup>	= 16,38 cm <sup>3</sup>			7100	
		1 liter	$= 1,0 \text{ dm}^3$	Accumulator size:			
Area		1 in <sup>2</sup>	$= 645,2 \text{ mm}^2$				1 10
		1 foot <sup>2</sup>	= 92900 mm <sup>2</sup>				V. × P <sub>1</sub>
Spee	d	1 km/h	= 0,2778 m/s				$V_x \times \frac{P_1}{P_0}$
		1 foot/s	= 0,3048  m/s	With slow charging a	nd slow d	ischarging V <sub>ac</sub> =	- 0
		1 mile/h	= 0,447 m/s				1- P <sub>1</sub> P <sub>2</sub>
Accel	eration	1 foot/s <sup>2</sup>	$= 0.3048 \text{ m/s}^2$				P <sub>2</sub>
Lengt		1 in	= 25,4 mm				
_5119		1 foot	= 0,3048 m				
		1 yd	= 0,9144 m				, P <sub>1</sub>
		i yu	- 0,01 77 111				V F1

# Pump:

Power consumption 
$$N_{an} = \frac{Q \times p}{600 \times \eta t}$$
 [kW]

Supplied oil capacity Q = 
$$\frac{q \times n \times \eta v}{1000}$$
 [l/min]

Input torque 
$$M = \frac{q \times p}{62.8 \times \eta m} [Nm]$$

With quick charging and quick discharging Vac =

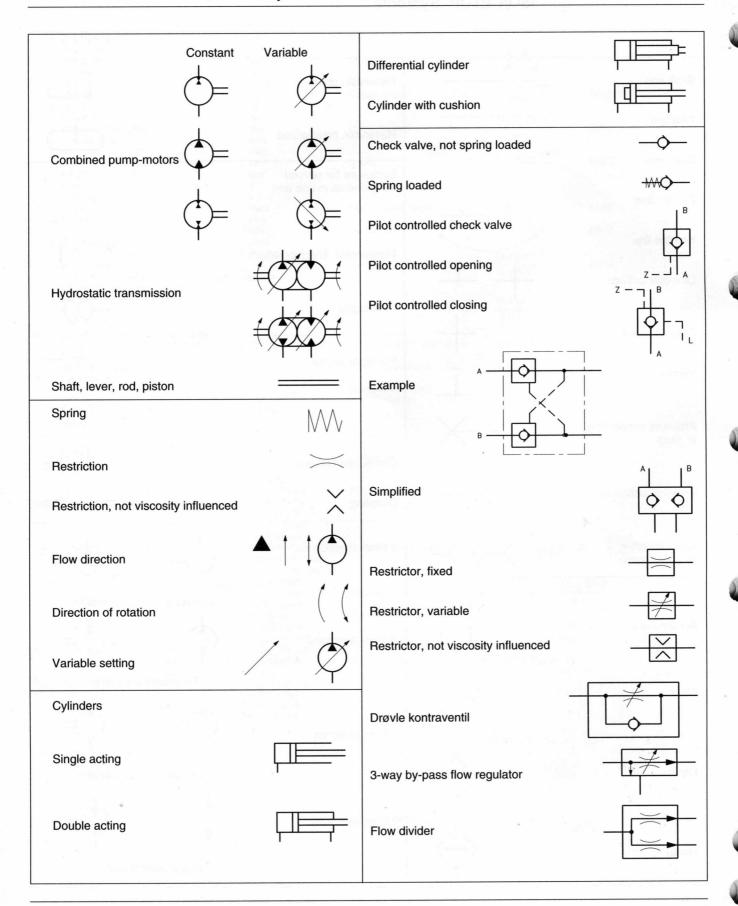
With slow charging and quick discharging  $V_{ac}$  =



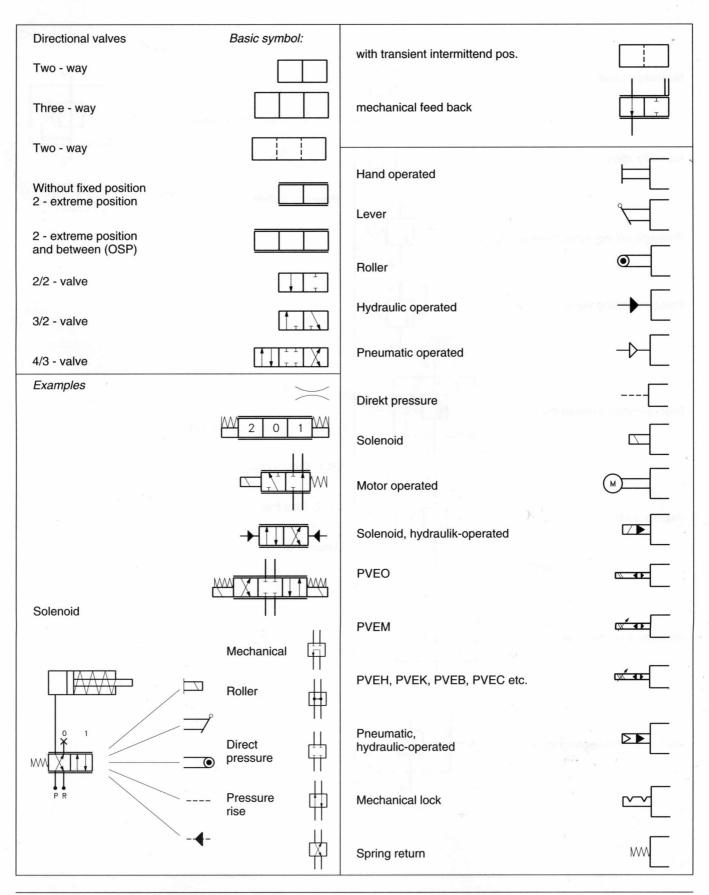
		1 Second	
Work line		Reservoir, open	
Pilot line		Reservoir, pressurized	
Drain line Electric line	4 4	Enclosure for several components in one unit	
Flexible line		Manometer, Thermometer	
Line connections  Corssing lines	+ + +	Flow meter	
Venting		Pressure source	•
Pressure connection	$\stackrel{\longleftarrow}{\longrightarrow}$	Electromotor	M
w. plug		Combustion engine	
With line connection	$\rightarrow$	Coupling	
Quick koupling w. check valve	$\longrightarrow + \longleftarrow \longrightarrow$	1 Flow direction	
Accumulator		2 Flow directions	Constant Variable
Filter			Displacement pump
		1 Flow direction	
Cooler		2 Flow directions	Constant Variable
Heater			Displacement motor

DKMH.PF.000.B1.22



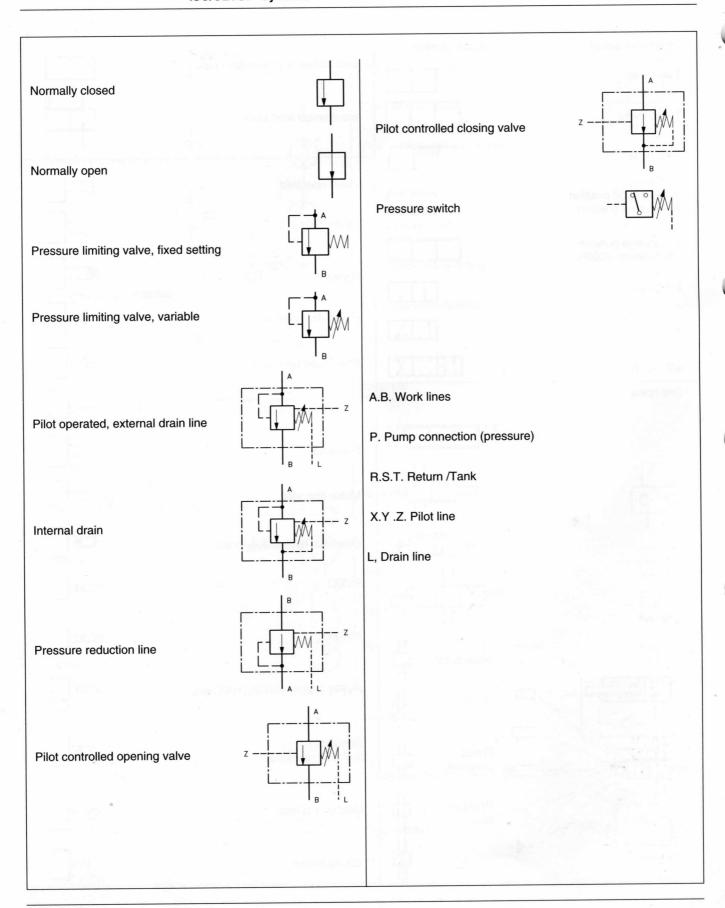






DKMH.PF.000.B1.22







Comments

Comments

DKMH.PF.000.B1.22



# Comments

Comments



Comments

Comments

DKMH.PF.000.B1.22



#### **Danfoss Hydraulics**

#### Catalogs or leaflets available for the following hydraulic components

Low speed hydraulic motors

Planetary gears

Hydrostatic steering units

Steering columns

Valve blocks

Flowamplifiers

Priority valves

· Torque amplifiers

Variable radial piston pumps

Pump controls

Gear wheel pumps for radial piston pumps

Proportional valves

· Remote control units

Electronics

Please contact the Danfoss Hydraulics sales organization for further information.

#### **Authorized service shops**

Australia

: Danfoss (Australia) Pty. Ltd., Melbourne

Austria Belgium Hainzl Industriesysteme, Gesellschaft m.b.H, Linz N.V. Danfoss S.A., Bruxelles

Canada Denmark Finland

Danfoss Mfg. Co. Ltd., Mississauga Danfoss Hydraulik A/S, Måløv

OY Danfoss AB, Espoo

France Germany **Great Britain** Iceland

Danfoss S.a.r.I., Trappes (Paris) Danfoss GmbH, Offenbach/Main Danfoss Limited, Greenford (London) Velsmidjan Hedinn H/F, Reykjavik

India Italy Japan

DANTAL HYDRAULICS PVT Ltd., New Delhi SORDELLA & C. Oleodinamica s.r.l., Moncalieri Danfoss K.K., Gotemba

**UNITEK Corporation, Seoul** Korea Netherlands New Zealand

ITHO B.V., Schiedam Danfoss (New Zealand) Limited, Auckland

Norway

Danfoss Norge A/S, Skui Republic of South Africa: Danfoss (Pty) Ltd., Johannesburg

Singapore Spain

Danfoss Industries Pte. Ltd., Singapore Danfoss S.A., San Sebastian de los Reyes

Sweden Switzerland Danfoss Hydraulik, Göteborg

U.S.A.

Danfoss Werner Kuster AG, Frenkendorf Danfoss Fluid Power Div. Racine, Wisconsin

# Service shops

Australia Australia Australia Danfoss (Australia) Pty. Ltd., Adelaide Danfoss (Australia) Pty. Ltd., Brisbane Danfoss (Australia) Pty. Ltd., Perth Danfoss (Australia) Pty. Ltd., Sydney

Australia Brazil

Danfoss do Brasil Ind.e Com. Ltda., Sao Paulo

Czech Rep. Greece

**TECHNO TRADE, Olomouc** A. SKOURA & Co. E.E., Athens

Israel New Zealand AZMA, Tel Aviv Danfoss (New Zealand) Limited, Christchurch

Portugal

Danfoss (Portugal), LDA, Lisboa Republic of South Africa: MERIDIAN Technologies (Pty) Ltd., Cape Town

Taiwan

SYMBRIDGE Machinery Co. Ltd., Taipei

Turkey

Mert Teknik Fabrika Malzemeleri Ticaret ve Sanayi A:S:, Istanbul

Danfoss can accept no responsibility for possible errors in catalogues, brochures and other printed material. Danfoss reserves the right to alter its products without notice. This also applies to products already on order provided that such alterations can be made without subsequential changes being necessary in specifications already agreed.

All trademarks in this material are property of the respective companies. Danfoss and the Danfoss logotype are trademarks of Danfoss A/S. All rights reserved.

**DK-6430 Nordborg Denmark**